

Date: March 7, 1994

To: Mr. Fred Austin

Puget Sound Air Pollution Control Agency

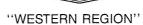
From: Gerald J. Brown

Subject: MEETING CONFIRMATION

Copy: Ken Rone Hans Steuch

This letter is to confirm our meeting with PSAPCA set for March 17, 1994 at 10:00 am.

Please inform me if any conflicts should arise.



Date: March 8, 1994

To: Ken Rone

Hans Steuch

From: Gerald J. Brown

Subject:Condition Report 03/08/94

Copy: Ed Pierce

Trygve Hille Matt Cohen

I called PSAPCA at 8:15 am to report an opacity excursion related to an undetermined cause believed to be associated with the main baghouse. I was told by the PSAPCA operator that PSAPCA is no longer taking calls of that nature but to write a letter about the condition and submit it with our month end CEM, report.

When previously informed of a letter by Jim Nolan, PSAPCA regarding this condition report policy, Mr. Commadvised that in order to claim the upset defense, excess emissions believed to be unavoidable needed to be reported by telephone as soon as it is realized that the emission resulted from a malfunction or other unavoidable upset conditions.

Ountil this matter is settled, I believe we should continue telephone reporting and document our efforts and the agency's response.

AGREE

"WESTERN REGION"

Date: March 18, 1994

To: Ken Rone

From: Gerald J. Brown

Subject: PSAPCA MEETING
March 17, 1994

Copy: Hans Steuch

Trygve Hille Ed Pierce Matt Cohen

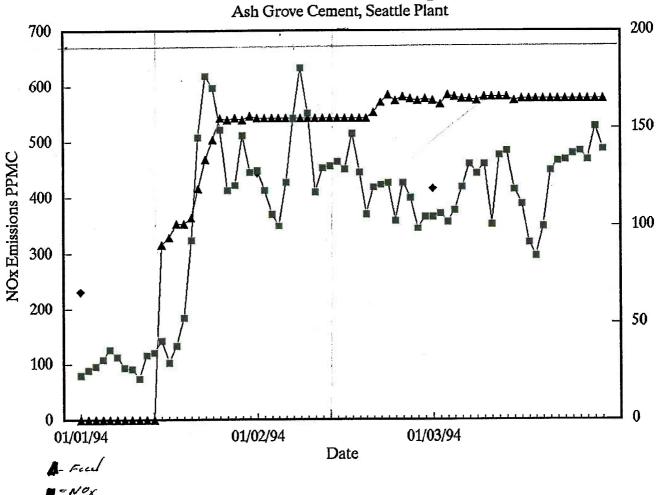
The meeting requested in our 01/21/94 response to Notice of Violation No. 32263 was held on March 17, 1994 to discuss compliance issues with PSAPCA. Those in attendance were Jay Willenberg and Fred Austin, PSAPCA. Ash Grove Cement Company was represented by Ken Rone, Trygve Hille, Hans Steuch, Jerry Brown, and Matt Cohen, Heller, Ehrman, White and McAuliffe. The following was discussed:

- 1. Defining kiln start up for exemption permit limits.

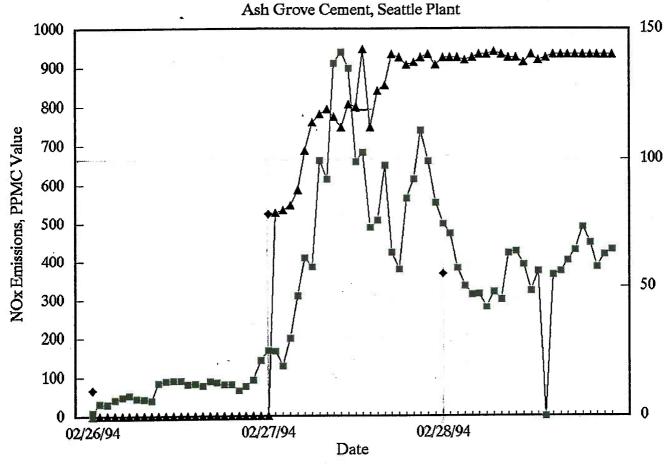
  It was requested that the PSAPCA permit is modified to exempt permitted limits during kiln start-up as stated in the PSD Application. PSAPCA was amenable to modifying the permit which sets new limits for startup as long as there is no increase in the annual emission rate. Ash Grove is to propose a permit amendment for emissions which justifies new limits and defines the startup period. In evaluating the startup scenario, all limits should be considered.
- 2. PPM and LBS/HOUR exceedances occurring simultaneously should not be separate violations.
  PSAPCA is willing to consider a new concentration level which will not cause an increase in the lbs/hour max limit. Ash Grove is to propose the wording which defines the single violation. This proposal may be applied to all permitted emission limits.
- 3. PSAPCA clarification of a CEM violation.
  PSAPCA will clarify to the community at a later date. Ash Grove will not report CEM Violations until instructed by PSAPCA to do so. The CEM-1 and CEM-2 reports will be changed to show periods of invalid CEM operation instead of CEM VIOLATIONS. Previously submitted CEM reports including November 1993 will be revised and submitted showing this change.

- 4. PSAPCA procedure for reporting upset conditions to qualify for the upset defense.
  PSAPCA will clarify in writing to the community. The Agency does not want telephone reports but will accept a fax or a written condition report for claiming upsets as soon as the cause has been determined.
- A new Notice of Violation will be issued based on the revised CEM reports for November and December 1993, January and February 1994. Any penalties resulting for these months, will be combined in a single proposed penalty. Work sheet showing penalty calculations will be provided by PSAPCA.

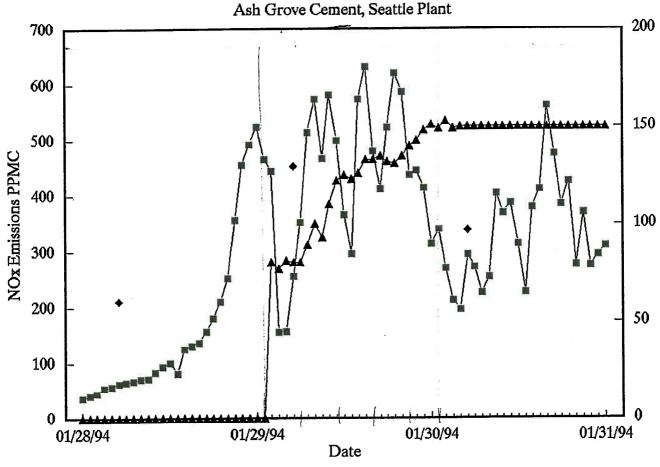
# NOx Emissions During Startup Ash Grove Cement, Seattle Plant



## NOx Emissions During Startup Ash Grove Cement, Seattle Plant



# NOx Emissions During Startup Ash Grove Cement, Seattle Plant



Date: March 17, 1994 Subject: PSAPCA MEETING

March 17, 1994, 10:00 am

1.	Status of current operations.
	When and why problems are occuring.
	New SO2 monitor.
2.6	PSAPCA clairfication of a CEM violation.
3.4	Start up NOx & SOx limits.
4.8	PPM and LBS/HOUR exceedances separate violations.
5.0	PSAPCA procedure for reporting upset conditions.
6. 4	Proposed penalties resulting from NOV.
	ATTENDANCE
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Sag	Willingburg
Matt	
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	- Propose a permit transformt.
	- Define seneris to include all at once.
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	enforce wording to 16 an south Violation
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#### PUGET SOUND AIR POLLUTION CONTROL AGENCY 110 Union Street, Suite 500 Seattle, WA 98101

COMPANY NAME:  Ash Groue  Gerry Brown  ADDRESS:  FAX:  SUBJECT:  Question: for May 9th Latter  Read these & Lets talk  Some before. We also need to  talk about "Penalty Worksheet" values.  SENT BY:  TODAY'S DATE: May 17 19984  Number of pages including this cover sheet:  2	(206) 343-8800	(800) 552-3565 FAX: (206) 343-7522
SUBJECT:  Question: for May 9th Letter  Question: for May 9th Letter  Acad these & Lets talk  SOME More. We also need to  talk about "Penalty Worksheet" values.  TODAY'S DATE: May 17 19984	ATTENTION:	6
COMMENTS:  Read these & Lets talk  Some more. We also need to  talk about "Penalty Worksheet" values.  SENT BY:  TODAY'S DATE: May 17 199 44	FAX:	623- 5355
talk about "Penalty Worksheet" values.  SENT BY:  TODAY'S DATE: May 17 199 44		Acad these & Lets talk
TODAY'S DATE: May 17 19967		talk about "Penalty Worksheet" values.
	TODAY	SDATE: May 17 199 67

Arthur Davidson, Acting Air Pollution Control Officer

## BOARD OF DIRECTORS

CHAIRMAN: Win Granlund, Commissioner, Kitsap County

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Norm Rice Mayor, Seattle Doug Sutherland Pierce County Executive Harold G. Moss. Mayor, Tacoma Gary Locke. King County Executive

Form No. 61-169 2/94

•	Questions concerning May 9th letter
	Are the stack pollutants 50:, CO, NOX & Oz measured wet or dry by CEM system.
	Compare PSD & PSAPCA limits.  Are they wet or dry standards?
	How much error is inherent in using a constant stack moisture for extended periods?  May need to install H2O CEM for moisture (Or wet/dry; NDIR; etc.) to statisty  Approval conditions for meditying NC 3382
	For CEM system rates the Agency has much move confidence with the use of source
	analyzer methods for future CEM system  Modif equations in Attachment 10 as needed for  wet / dry conversions as needed.
	Wet / dry conveysions as needed.  Use CEM to measure (ppm); (Oz); (H2O); Q  to calculate 16/hr emission rates and compare with standards (50z=40/4hr); (00=538/4hr); (NOx=590/6/hr); (NOX = 422/6/24hr)



KING COUNTY

SOUND

AIR KITSAP COUNTY

PIERCE COUNTY

POLLUTION

SNOHOMISH COUNTY

June 1, 1994

Gerald J. Brown Manager, Safety and Environment Ash Grove Cement Company 3801 East Marginal Way South Seattle, WA 98134

Dear Mr. Brown:

#### Ash Grove Cement Company

A review of our May 18, 1994 letter requesting revisions to Notice of Construction No. 3382 has prompted the following questions and comments. Some of these questions were sent via FAX to you on May 17, 1994.

- Check the methods used by Ash Grove to measure the stack emissions to find if these methods provide wet or dry measurements.
- Compare the requirements of PSAPCA and the PSD permit and make sure the reported emissions of the PSAPCA limits are on a dry standard basis.
- Check that the SO<sub>2</sub> Relative Accuracy Test Audit (RATA) calculations have been corrected to dry standard conditions.
- A question raised in a previous letter concerns the error inherent in using a constant stack (D) moisture for extended periods of time for emission corrections to dry conditions. Please quantify the error associated with the use of an assumed H2O percent for reporting the emission calculations and compare with the use of a wet/dry continuous monitoring device.
- Modify the equations in "Attachment 10" as needed to reflect dry conditions. (E)
- The Agency has reviewed the SO<sub>2</sub> RATA performed using Method 6 and finds it acceptable. For future tests, will Ash Grove use analyzer methods (i.e. Method 6C or 7E) for performing the annual re-certification tests?
- Notice of Violation (NOV) No. 31785 issued May 6, 1994 was for fugitive emissions from the kiln seal during startup when the kiln was rotating. Fugitive dust was also seen from the plant during the weekend of May 22, 1994. There is a scheduled inspection on June 9, 1994 to observe the operation of the kiln seals during startup. These fugitive dust problems have

Arthur Davidson, Acting Air Pollution Control Officer

O F DIRECTOR BOARD

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(206) 343-8800

Harold G. Moss, Mayor, Tacoma Norman B. Rice, Mayor, Seattle Doug Sutherland, Pierce County Executive June 1, 1994
Page 2

generally not been observed during previous startup cycles. The Agency is concerned about this apparent fundamental change in emissions.

- (i) The Ash Grove letter of May 18, 1994 indicates these fugitive dust emissions "could not be avoided." However, Ash Grove attached a letter from Fuller (June 29, 1992) which states, "When an upset condition occurs in the process which requires that kiln and I. D. fan be stopped, it is possible that some dust may be released through openings at the discharge hood." The reference is when the kiln and I. D. fan are stopped, but NOV No. 31785 occurred when the kiln was turning.
- (ii) Also, the Fuller letter indicates additional venting at the G-cooler could be installed to control dust "irrespective of whether the kiln is running or not." Has this additional venting been installed?

The revisions to the Ash Grove permit will not be retroactively applied. Notices of violation are being issued for the emissions exceeding the limits as measured by the CEM system during the first quarter of 1994.

Please provide the requested information in order to allow the processing of your permit revision request.

Please contact me at 689-4055 or FAX 343-7522 if you have any questions.

Very truly yours,

Fred L. Austin

Air Pollution Engineer

mj

cc D. S. Kircher

J. M. Willenberg

R. G. Busterna

T. J. Hudson



3801 EAST MARGINAL WAY, SOUTH SEATTLE, WA 98134 PLANT OFFICE: (206) 623-5596 FAX: (206) 623-5355

TELECOPIER TRANSMISSION REPORT

DATE: 6/16/99	
TO: Hans Steach	<b>'</b>
COMPANY:	· · · · · · · · · · · · · · · · · · ·
FROM: O Wroun	
SUBJECT:	
NUMBER OF PAGES (including	cover):
Fred Says:	
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12/9	3 7 1/94/- 2/94.
COMMENTS: Thes	e number : eve preliminary
for	the Civil Penalty.
	c Review & add any into
SENT BY:	Fred Austin
TODAY'S DATE:	4-26-94
Number of pages includi	ng this cover sheet:



Table I  Gravity Criteria  Table I  Gravity Criteria  No (0) Possibly (1) Probably (2) Definitely  1. Did the violation result in air pollution?  Was it a willful or knowing violation?  Was the violator unresponsive in correcting the violation?  Was the violation a result of improper operation or inadequate maintenance?  5. Did the violator have a history of similar violations?  6. Did the violator benefit economically from noncompliance?  Total Gravity Criteria Rating  H + #2
1. Did the violation result in air pollution?  2) Was it a willful or knowing violation?  3. Was the violator unresponsive in correcting the violation?  4. Was the violation a result of improper operation or inadequate maintenance?  5. Did the violator have a history of similar violations?  6. Did the violator benefit economically from noncompliance?  Total Gravity Criteria Rating  No (0) Possibly (1) Probably (2) Definitely
1. Did the violation result in air pollution?  2 Was it a willful or knowing violation?  3. Was the violator unresponsive in correcting the violation?  4. Was the violation a result of improper operation or inadequate maintenance?  5. Did the violator have a history of similar violations?  6. Did the violator benefit economically from noncompliance?  Total Gravity Criteria Rating  4 + #2
Table II
Gravity Component Penalty
Rating: 1-4 5-7 8-9 10 11 12 13 14 15 16+ Penalty: **** \$1,000 ***\$2,000 * \$3,000 \$4,000 \$5,000 \$6,000 \$7,000 \$8,000 \$9,000 \$10,00
Benefit Component Penalty
If the answer to question #6 in Table I is "Definitely", the estimated dollar amount of economic benefit determine
EPA BEN computer model is: \$ (attach calculations).  Comments: See Attach worksheets which are copies of
the Asharove CEM daily violation reports
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CO = 1000 ppm/hr \$ 2 000 = 538 b/hr \$ 0
7-20-000 26-000
7 20 000
Evaluator: Date: Civil Penalty Recommendation: \$26,000
Checked By: Date:

### 1. Did the violation result in air pollution?

Answer "no" if the violation was not the result of an emission. Use the following table if an emission standard was violated:

Percent Above Emission Standard	Rating
1-24%	0
25-99%	1
100-199%	2
>200%	3

#### 2. Was it a willful or knowing violation?

Answer "no" if the violator obviously did not know that the action or inaction constituted a violation. Answer "possibly" if it is likely the violator knew. Answer "probably" if the violator should have known. Answer "definitely" if the violator clearly knew.

### 3. Was the violator unresponsive in correcting the violation?

Answer "no" if the violation was corrected as soon as the violator learned of it. Answer "possibly" if the violation was corrected in a less timely and cooperative fashion. Answer "probably" if the violator attempted to correct the problem, but did not correct it. Answer "definitely" if the violator did not attempt to correct the problem.

## 4. Was the violation a result of improper operation or inadequate maintenance?

Answer "no" if the violator was following an acceptable O & M plan. Answer "possibly" if the violator was following an O & M plan that was not adequate. Answer "probably" if the violator did not have an O & M plan. Answer "definitely" if the violator did not have an O & M plan and the violation was clearly a result of improper O & M.

#### 5. Did the violator have a history of similar violations?

Answer "no" if the violation did not occur previously. Answer "possibly" if the violation may have occurred before, but has not been previously cited. Answer "probably" if the violation occurred previously, but had not been previously cited. Answer "definitely" if the violation had been previously cited.

## 6. Did the violator benefit economically from noncompliance?

Answer "no" if the violator clearly did not obtain any economic benefit. Answer "possibly" if the violator may have benefited. Answer "probably" if the violator benefited, but the benefit is not quantifiable. Answer "definitely" if the economic benefit to the violator is quantifiable.

Form No. 80-226 (4/30/92)

RECEIVED

Form CEM-1

#### PUGET SOUND AIR POLLUTION CONTROL AGENCY

JAN 0 3 1994

**ENGINEERING DIVISION** 

110 UNION STREET, SUITE 500, SEATTLE, WA 98101

Puget sound air pollution Rescribed Ageney, (206)689-4405

Month of November 1993

#### CEM - MONTHLY SUMMARY REPORT

Date Recieved:		- 19-1			•
Name:	Ash Grove Cement Co.  3801 E Marginal Way S	City:	Scuttle, W A 98134		•
Contact	Jon Trygre Hille	•		Tele #:	(206) 623 - 5596
Baric Equip went:	Cement Kiln				
Control Equipment	Dry Scrubber Baghouse				
CEM Equipment:	Continuom Emission Monitors			•	

Complete a Form CEM-2 for each parameter checked below:

			_*	٠.	584104	
		Make & Model	Allowed Limit	CEM Violations	Violations	. :
	Opacity	Lear Siegler	20% @ 1 br	. 0		
		Dynatron 1106 M	5% <b>@</b> 3 min		•	'
Z	SO2	Lear Siegler	33 pp mc @ 1 hr -	3	79	
		3960	40 15/br @ 1 br		150	
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	Flow	EMRC	t/a	8	g/a	
	•			15	270	Tota

Total = 285.

Attent a supplemental report for each amission violation and for each violation of monitoring requirements (e.g. less than 90% valid boars of daily monitoring). Violations are subject to PSAPCA coforcement actions, including civil penalties of up to \$10,000 per day

QUARTERLY (OR RATA) CERTIFICATION TESTING:

Last Completed Passed Failed Next Scheduled

RATA Certification 11/13/93 O2.NOz.CO.Flow SO2

Quely Certification . None

I hereby certify the attached information is true and accurate to the best of my knowledge.

12/29/93 Date

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24.0         24.0         26.0         25.0         21.0         74.0         0.0         0.0         24.0         0.0         24.0         0.0         24.0         0.0         24.0         0.0         24.0         0.0         24.0         0.0         24.0         0.0         24.0         0.0         0.0         24.0         0.0		16.0			1		_								1
24.0         24.0         0.0         24.0         69.0         0.0         0.0         0.0         No           24.0         24.0         1.0         36.3         8.0         8.0         80.0         0.0         0.0         0.0         No           24.0         25.0         79.0         110.0         36.0         97.0         30         0.0         164.0         0.0         No         0.0 <t< td=""><td>186</td><td>TVG.</td><td></td><td></td><td>6</td><td></td><td>_</td><td></td><td></td><td>•</td><td></td><td></td><td></td><td></td><td>1</td></t<>	186	TVG.			6		_			•					1
24.0         24.0         1.0         38.8         8.0         8.0         80.0         90	100	186									•				200
281.0		246			c		2								
2810   258.0	2 2	119%										lo l			#
		281	1									0		/w //	2000
	5														ĺ

Hours   Hour	House   Hous	meter Monitored: NOx	×i	اسوا	·2	I Carabby Court	FORM CEM-2	-Z-	•		ı	<u>.</u> .	Quarter: 4	4th	21
Hours   Exceed   Exceed   Exceed   Fourty   Maillington   Houry   Maillington   Houry   Fine   Houry   Maillington   Houry	Houre Exceed Houry Exceed Houry Mallinneon Hours Will World Houry Houry Mallinneon Hours Will World Houry Hours H	-		Houre	Houre	Max	House	Houre	Max	H	2				
Colored   Colo			To La	Exceed	Exceed.	Hourty	1 horr	Exosed 1 day	Hourly	Mailun	Gron	Hours Viol.	\$ 5 \$ 5	8	200
				potro fim.	pama (Im.	Reading	D/hr lm.	. •	Reading						
		1								1 1					
Columbia   Columbia	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1		•		c			VOY	701					
24.0         0.0 <td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td> <td>1</td> <td></td> <td>1</td> <td></td> <td>6</td> <td>1400</td> <td></td> <td>2</td> <td>141</td> <td>1</td> <td></td> <td></td> <td></td> <td>Į</td>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1		1		6	1400		2	141	1				Į
28.0         0.0 <td>24.0</td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	24.0	1							-						
24.0         0.0 <td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td> <td>1</td> <td></td> <td>i I</td> <td></td> <td></td>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1											i I		
24.0         0.0         0.0         596.B         0.0         485.D         0.0         0.0         0.0         Vee           24.0         0.0         0.0         495.D         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           14.0	24.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1													
24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           4.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           5.0         0.0         0.0         0.0         0.0         0.0         Vee           7.0         0.0         0.0         0.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0<	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+	T	ŀ											J.
24.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           2.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           2.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           2.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           2.0         0.0         0.0         0.0         0.0         0.0         0.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Ļ	T												
24.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           7.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           2.0         0.0<	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+													
24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           7.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0         0.0         0.0         0.0         Ve	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+													
24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0	24.0	Ł													
24.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           6.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           7.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           7.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           7.0         0.0         0.0         0.0         0.0         0.0         Vee           7.0         0.0         0.0         0.0         0.0         0.0         Vee           7.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0           2.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	╀													0
24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           5.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           5.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           6.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           7.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0         4780         1.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0         4780         2.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0         4780         0.0         0.0         0.0         Vee           2.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           2.0         0.0         0.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6	24.0	00	00	596.8		0.0			0.0	0.0	0.0	Yes	2
50         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           40         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           71.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           23.0         1.0         0.0         0.0         0.0         0.0         0.0         Vee           23.0         1.0         0.0         0.0         0.0         0.0         0.0         Vee           23.0         1.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           14.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           15.0         0.0 <td< td=""><td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td>F</td><td>24.0</td><td>0.0</td><td></td><td>627.8</td><td></td><td>0.0</td><td>_</td><td></td><td>0.0</td><td>0.0</td><td>0.0</td><td>Veo</td><td>2</td></td<>	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	F	24.0	0.0		627.8		0.0	_		0.0	0.0	0.0	Veo	2
0.0         0.0         0.0         0.0         0.0         0.0         √ee           V1.0         2.0         0.0         0.0         0.0         0.0         √ee           V1.0         2.0         0.0         0.0         0.0         0.0         Vee           V1.0         2.0         0.0         0.0         0.0         0.0         Vee           23.0         0.0         0.0         4.0         0.0         0.0         0.0         Vee           23.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           10         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee           10         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Vee	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	20	00		273.3	-	0.0	2		0.0	0.0	0.0		Ž
V1.0         Z0         C0         B59.8         1.0 S         C0 O M M M M M M M M M M M M M M M M M M	110   20   0.0   689.8   1.0   0.0   478.0   1.0   0.0	0	00	00		0.0						0.0	0.0		Š
23.0         1.0         0.0         680.0         0.0         478.0         1.0         0.0         2.0         0.0         Yes           22.0         0.0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6	0.17	20		B.659.B		0				2.0	0.0		Ž
22.0         0.0         0.0         2.0         0.0         Ves           24.0         0.0         0.0         0.0         0.0         0.0         Ves           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           14.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           14.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           0.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           15.0         0.0         0.0         0.0         0.0         0.0         <	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	F	23.0			0.089						2.0	0.0		Ž
24.0         0.0         0.0         0.0         0.0         0.0         0.0         V****           14.0         0.0 </td <td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td> <td>6</td> <td>022</td> <td></td> <td></td> <td>586.8</td> <td></td> <td></td> <td></td> <td></td> <td>100</td> <td>2.0</td> <td>0.0</td> <td></td> <td>2</td>	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6	022			586.8					100	2.0	0.0		2
14.0 $0.0$ <	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	, to	24.0			233.3						0.0	0.0		Ŝ.
0.0         0.0 </td <td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td> <td>1</td> <td>14.0</td> <td></td> <td></td> <td>214.3</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.0</td> <td></td> <td></td> <td>Ž</td>	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	14.0			214.3						0.0			Ž
Ho   Ho   Ho   Ho   Ho   Ho   Ho   Ho	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6	00			74.0						0.0			Š
15.0   2.0   0.0   909.3   1.0   0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6	0.0			849.0			,			6.0			2
0.0         0.0 <td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td> <td>6</td> <td>15.0</td> <td></td> <td></td> <td>909.3</td> <td></td> <td>0</td> <td></td> <td></td> <td></td> <td>2.0</td> <td></td> <td></td> <td>2</td>	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6	15.0			909.3		0				2.0			2
0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           16.0         6.0         0.0         9.0         9.0         0.0         0.0         Ves           24.0         6.0         0.0         0.0         0.0         0.0         0.0         Ves           24.0         1.0         84.1         2.0         0.0         0.0         0.0         0.0         Ves           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           25.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           25.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           25.0         0.0         0.0         0.0         0.0         0.0         Ves           25.0         0.0         0.0         0.0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	e	00			0.0						0.0			S
16.0         6.0         0.0         913.3         3.0         0.0         6.0         0.0         6.0         0.0         Yes           24.0         13.0         1.0         841.8         2.0         0.0         0.0         0.0         0.0         0.0         Yes           24.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           25.0	16.0         6.0         0.0         913.3         3.0         0.0         6.0         0.0         6.0         0.0 $Y_{00}$ 24.0         13.0         1.0 <t< td=""><td>6</td><td>00</td><td></td><td></td><td>0.0</td><td></td><td></td><td></td><td></td><td></td><td>0.0</td><td></td><td></td><td>Ŝ</td></t<>	6	00			0.0						0.0			Ŝ
Z4.0         13.0   1.0   841.8         Z0   0.0         1.0   851.0         Ve*           Z4.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Ve*           Z4.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Ve*           Z4.0         0.0         0.0         0.0         0.0         0.0         0.0         Ve*           Z58.0         30.0         1.0         949.0         7.0         1.0         658.0         3.0         0.0         33.0         1.0           Z58.0         30.0         1.0         949.0         7.0         1.0         658.0         3.0         0.0         33.0         1.0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	E	160		<u> </u>	913.3		0	Į.			0.9			S N
Z4.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Ve*           Z4.0         0.0 <td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td> <td>E</td> <td>240</td> <td></td> <td></td> <td></td> <td></td> <td>0</td> <td></td> <td></td> <td></td> <td>13.0</td> <td></td> <td></td> <td>2</td>	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	E	240					0				13.0			2
24.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         Ves           258.0         30.0         1.0         949.0         7.0         1.0         658.0         3.0         0.0         33.0         1.0           258.0         30.0         1.0         949.0         7.0         1.0         658.0         3.0         0.0         33.0         1.0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	t	DAG.						L			0.0			2
258.0 30.0 1.0 949.0 7.0 1.0 658.0 3.0 0.0 33.0 1.0 1.0 258.0 3.0 0.0 33.0 1.0	$\frac{2580}{2580}$ $\frac{300}{300}$ $\frac{10}{10}$ $\frac{9490}{9490}$ $\frac{70}{70}$ $\frac{10}{10}$ $\frac{6580}{6580}$ $\frac{30}{30}$ $\frac{00}{40}$ $\frac{330}{330}$ $\frac{10}{10}$	te	2411											1	2
258.0 30.0 1.0 949.0 7.0 1.0 658.0 3.0 0.0	2580 300 10 949.0 10 00 00 00 00 00 00 00 00 00 00 00 00	非					ŀ								
	= 1 Cate 10 #2+ 40011 = 5 points =	2	2580			949.0							1.0		

g	Offic	Teel												Ŝ	Š	2	2	2	Ž	2	2	2	0	0 4	2 4	0 4	2 4	20	OM	Š				
November 1993 4th	Daily	Calib.		1		$\frac{1}{ }$	ŀ							Yea	B <b>⊕</b> A	Yes	Yee	Yee	Yes	\$ \ \	\$6 /	X 6.8	7.00	, A	i i	100	00 /	80	¥ 68	Y65	Yes			8
Month: No	Daye In	Violation					-		-					0.0 ,	0.0	0.0	000	0.0	0:0	00	O.O.	D'A	000	0.0	28	200	300	20	20	n'o	00	0.0	0.0	<b>#</b> 2000
<b>₹</b> ∂	L	Z S			1	1	+							0'0	101	0.0	0.0	0.0	0:1	2.0	2	2.0	2,5	2.5	2,6	2,5	28	3	3	8	00	4.0	4.0	介
· ·	· · ·	Equip				+			-					00	0.0	0:0	0.0	0.0	0.0	0.0	000	200	200	30	200	0.0	0.0	O'O	0.0	0.0	0.0	0:0	0.0	6 points
	Malfunction	CEM								<u> </u>				0.0	0.0	0.0	00	0.0	1.0	2.0	0.0	0.0	00	000	0.5	2.0	3.0	200	00	0.0	0:0	30	0'E	12
	Max	Beading			Const	7 250				<del> </del>				285.0	485.0	425.0	1.0	240.0	274.0	326.0	329.0	319.0	0.1	59.0	0.03	9.	0,1	247.0	273.0	276.0	253.0	485.0	485.0	+ 40014
FORM CEM-2	Times	b Hour				m d					ľ			0.0	12.	00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	00	00	0.0		0.0		·		0.1	#2+
Figure 6 and 1	Max 8 Heur	ppmo			ļ	1000 P	7	ľ						١		2005						658.5		309.6			302.3					1208.1		Criteria
	Fygged							1		Ī				00	P	00	00	0.0	00	6	00	0.0	0.0	0,0	0.0	0.0	00	0.0	0.0	0.0	0.0	0.1	<u>P</u>	
	Horas	Ž					1			1				24.0	24010	_	00	011	23.0	22.0	24.0	14.0	0.0	0.0	15,0	00	0.0	16.0	24.0	24.0	24.0	258.0	258.0	Gravity
ored: CO	House	Oper							1	1	+			076	24.0	50	00	1011	240	24.0	24.0	14.0	0.0	8.0	15.0	0.0	0.0	16.0	24.0	24.0	24.0	2810	0.185	
ameter Monitored:		Ogy	11881	11/02	11/03	11/04	90	2	100	200		4.4.4	6//	11/13	ZI/LI	11/15	11/18		11/18	11/19	11/20	11/21	11/22	11/23	11/24	11/25	11/26	1/2/1	11/28	11/29	11/30	Tolai	QLO	h1/11

•	•		Patino
502 9/27	1799	80%	
10/05	2113	111%	
10/06	2060	106%	
10/20	1502	50 %	1
10/24	1105	11%	0
	1130	13%	0
10/29	163.4	63%	
11/26	1056	6%	0
11/18	1294	29%	11
11/19	1787	79%	1
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